

## Homework 5

Assigned Friday March 4, Due Monday March 14, 2022

10 pts total

- 1) 1 points, Propellant Performance
- 2) 2 points, Combustor Cooling
- 3) 1 points, Combustor Geometry
- 4) 2 points, Combustor Pressure, Injector Design
- 5) 2 points, Optimal Performance
- 6) 2 pts Conical Nozzle Correction

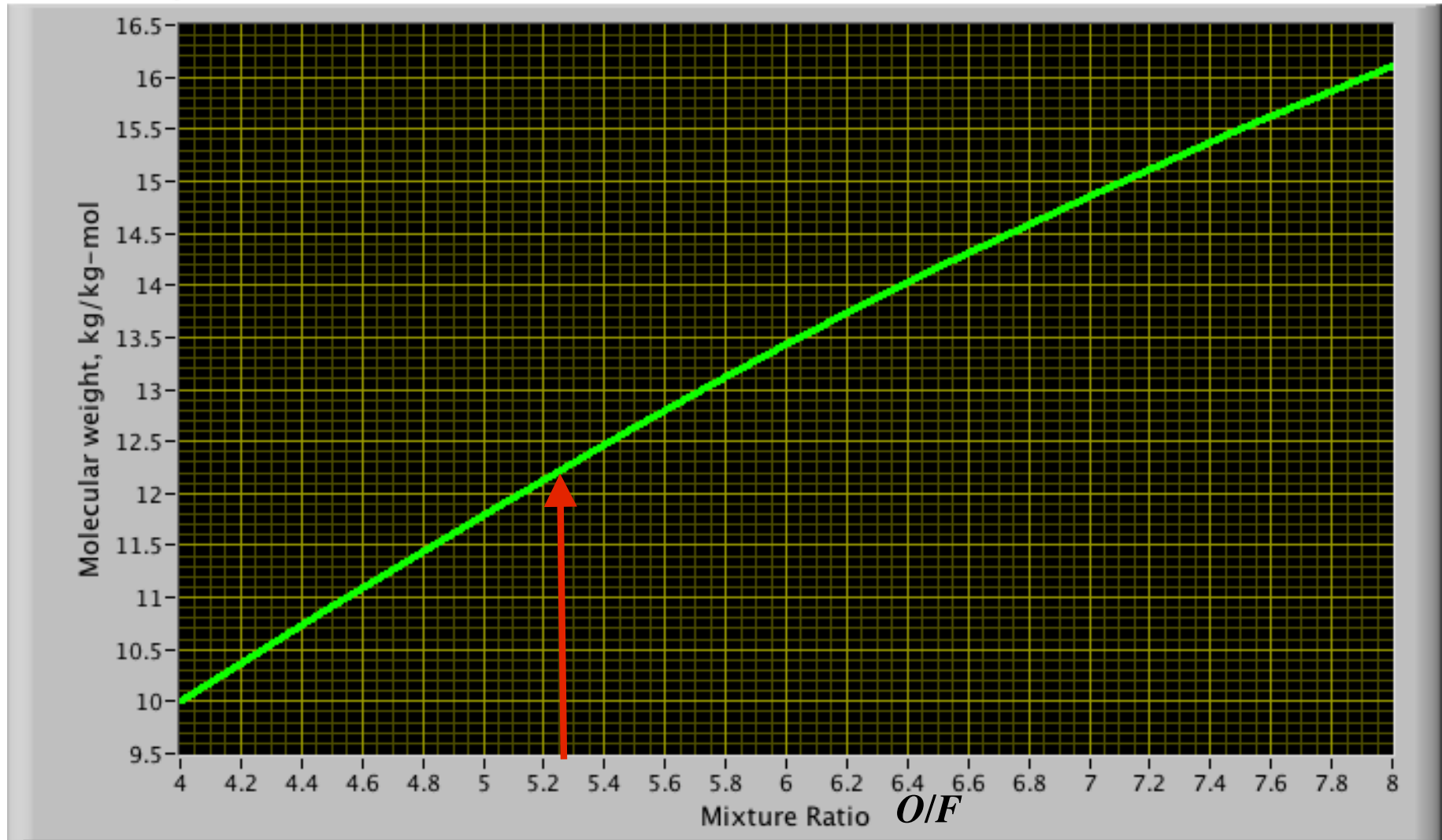
## 1) Propellant Performance (1 Point)

- A Bi-Propellant Rocket Engine Burns  
LOX/LH<sub>2</sub> ... with an O/F ratio of 5.33333

*... compute the Ideal characteristic velocity,  $C^*$   
and Maximum ideal specific impulse (infinite expansion nozzle)*

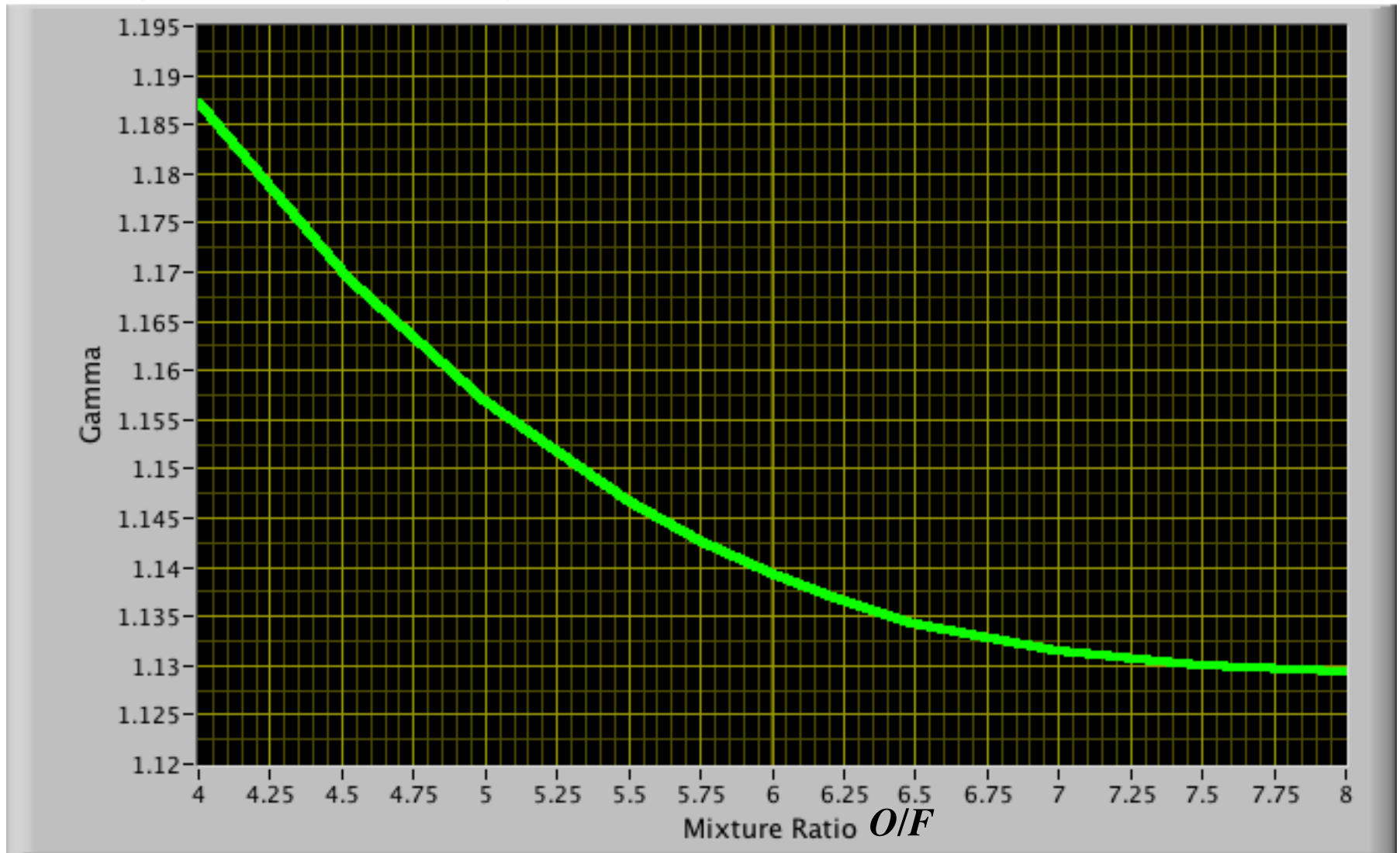
# Propellant Combustion Properties

Molecular Weight of Idealized Combustion Products



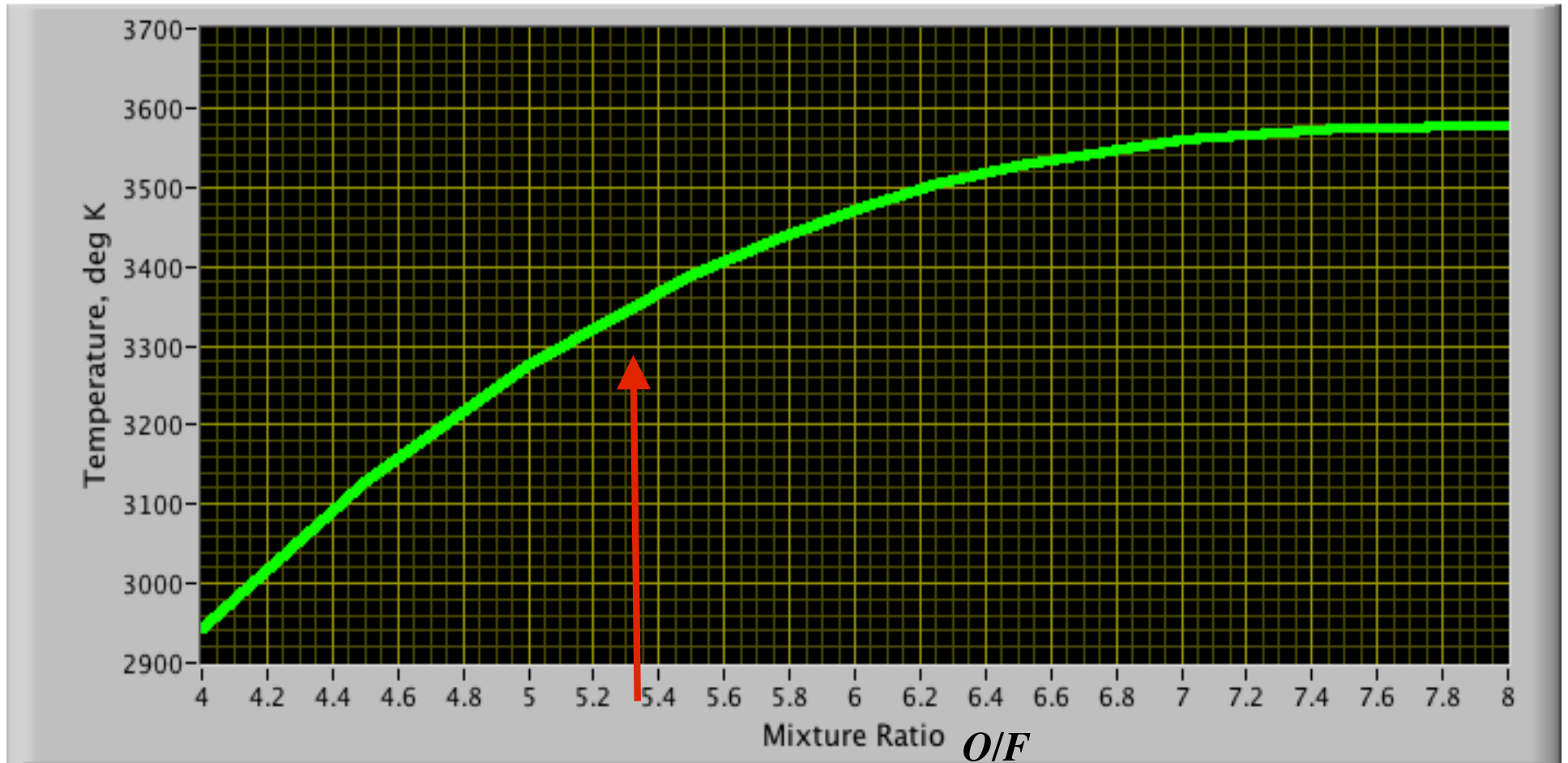
# Propellant Combustion Properties

Idealized Specific heat ratio of Combustion products



# Propellant Combustion Properties

Adiabatic Flame (Ideal Combustor) temperature



## 2) Non-Ideal Combustion Temperature (1 point)

- For the same Rocket in (1) ... Assume that there is regenerative cooling in the combustor .....

When operating in steady state mode  
The regenerative cooling system removes  
700 kWatts / kg/sec of propellant mass flow  
entering the combustor

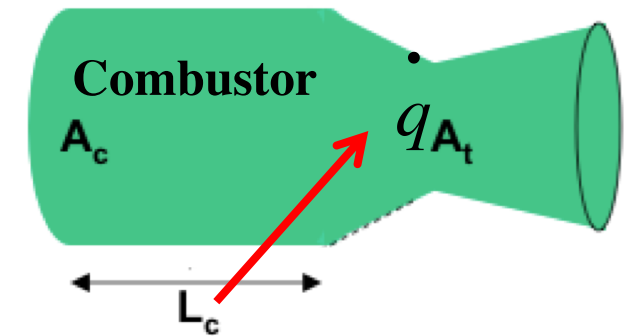
$$\text{Assume } \rightarrow h_{0_{actual}} = h_{0_{ideal}} - \left( \frac{\dot{q}}{\dot{m}} \right)_{cooling} \rightarrow h \approx c_p \cdot T$$

**Calculate the actual stagnation temperature at the throat of the combustor and the efficiency of the combustion-->**

$$\eta^* = \frac{1}{C^*_{ideal}} \cdot \left( \frac{P_0 \cdot A^*}{\dot{m}} \right) = \frac{C^*_{actual}}{C^*_{ideal}}$$

Assume that heat transfer has no effect on combustion products and that  
Flow is “frozen” with species mix defined at O/F = 5.333

**Combustor Geometry**



### 3) Combustor Geometry

- For the same Rocket in (1), (2), and (3) ...

Ranges of Combustor Characteristic Length

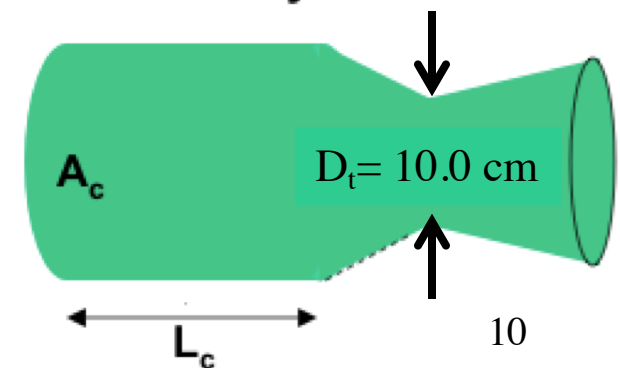
Propellants	Characteristic Length $L^*$	
	Low(m)	High(m)
Liquid fluorine / hydrazine	0.61	0.71
Liquid fluorine / gaseous $H_2$	0.56	0.66
Liquid fluorine / liquid $H_2$	0.64	0.76
Nitric acid/hydrazine	0.76	0.89
$N_2O_4$ / hydrazine	0.60	0.89
Liquid $O_2$ / ammonia	0.76	1.02
Liquid $O_2$ / gaseous $H_2$	0.56	0.71
Liquid $O_2$ / liquid $H_2$	0.76	1.02
Liquid $O_2$ / RP-1	1.02	1.27
$H_2O_2$ / RP-1 (incl. catalyst)	1.52	1.78

- Given the following Characteristic length Values,

*Calculate a mid range value for The combustor Volume based on*

$$L^*_{mean} = \frac{L^*_{high} + L^*_{low}}{2}$$

#### Combustor Geometry



## 4) Steady Combustor Pressure

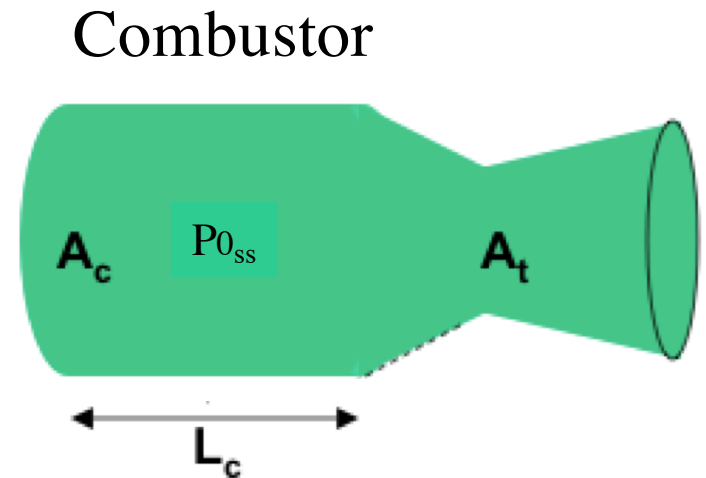
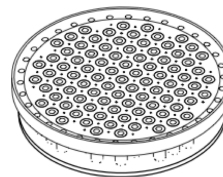
- For the same Rocket in (1), (2), and (3), and the combustor geometry from (4) ... Use the true stagnation temperature calculated in (3), and assume that the combustion products are frozen as in (1) ... for the following injector properties .. **Calculate the steady state combustor pressure (assume incompressible propellants)**
- **What LOX Injector feed pressure is require to give  $O/F$  5.33333**

- **LOX Injector**

Port diameter: 0.1841 cm  
 100 injector ports  
 LOX density:  $1.140 \text{ g/m}^3$   
 Cd (discharge coeff.): 0.75

- **LH<sub>2</sub> Injector**

Port diameter: 0.1596 cm  
 100 injector ports  
 LH<sub>2</sub> density:  $0.071 \text{ g/cm}^3$   
**Injector pressure 3700 kPa**  
 Cd (discharge coeff.): 0.75



**Base calculations on actual combustor temperature**



## 5) Design Specific impulse

- Given the results of problem (1), (2), (3), (4), (5)

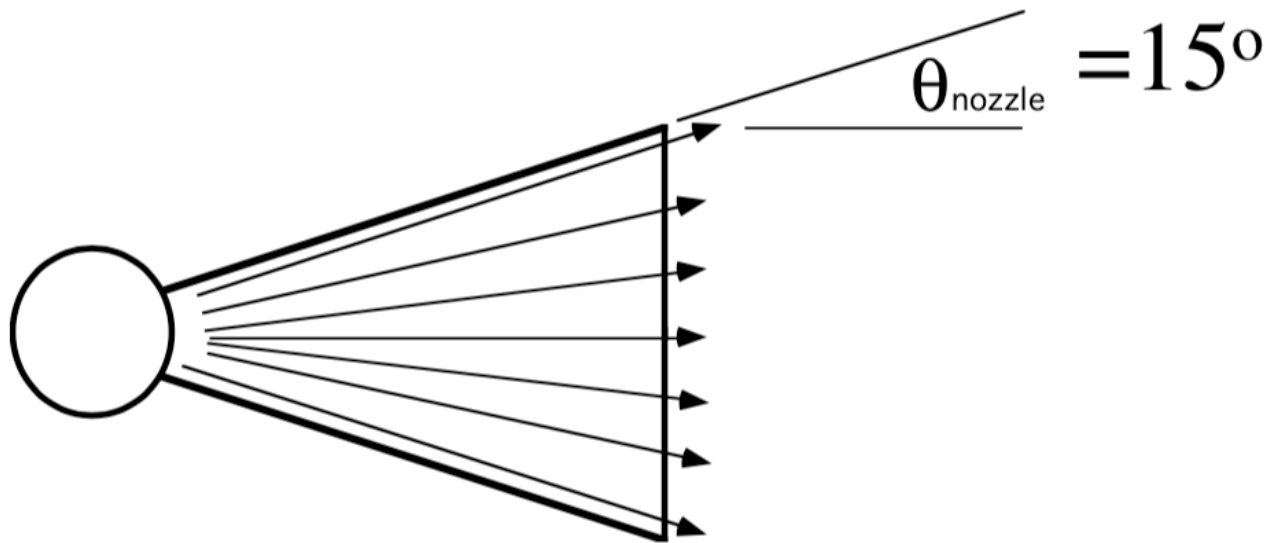
*calculate the Optimal (design) Specific Impulse, Thrust Coefficient, and Total Thrust when the nozzle has a design altitude of 20 km ( $p_{amb} = 5.4748$  kPa)*

.... Assume nozzle exit divergence angle is zero, *be sure to include effects of combustor heat loss*

*Calculate the expansion ratio of this optimal nozzle*

## 6) Nozzle Exit Angle Correction

- Now Consider a conical nozzle of same expansion ratio, but with a  $15^\circ$  exit angle,



- How does this exit condition *qualitatively and quantitatively* affect the engine Isp, CF and total Thrust the design operating altitude?