

Major Project 1 ... **16 Points Total!**

- Look at problem of transferring satellite to MEO (GPS) from Initial LEO Orbit

- Code Continuous Thrust Example
- ALEO ~ 8530 km
- AMEO $\sim 13,200$ km
- Isp ~ 2000 sec
- Thrust ~ 10 Nt

... Implement both Trapezoidal and Runge-Kutta Integration schemes

... compare algorithm performance as Time interval becomes progressively larger

- Include a *Thrust Termination* Criterion which puts you in the proper final transfer orbit (apogee tangent to desired MEO Orbit)
- Calculate Impulse ΔV and Propellant Mass Required to Circularize Final Orbit

for continuous thrust problem .. assume final delta V is delivered impulsively with Apogee Kick Motor Isp = 270 sec Ignore atmospheric drag

a.1) Continuous Small Thrust, Simulation (6 pts)

Terminate thrust when

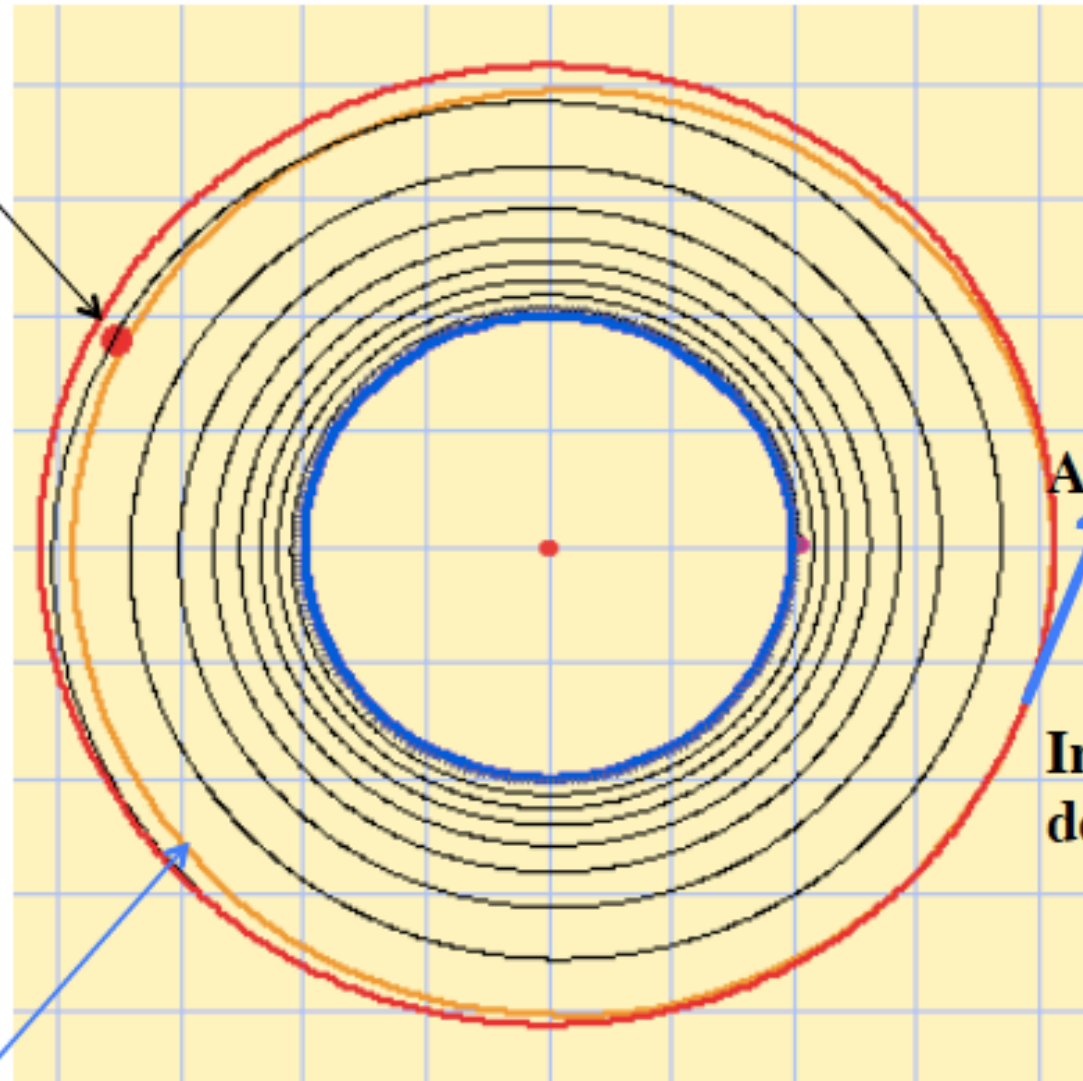
$$R_{apogee} = a \cdot (1 + e)$$

$$= 13,200 \text{ km}$$

Calculate:

- 1) Propellant mass req.
For continuous transfer
- 2) Propellant mass req.
For kick delta V (*impulsive*)
(orbit circularization)
- 3) Final mass = 1000 kg

Orbit coast



Assume

$$\Delta V_{kick} @ 270_{sec} I_{sp}$$

Impulsively
delivered

a.2) Continuous Small Thrust (*1 pt*)

... Implement *both* Trapezoidal and Runge-Kutta Integration schemes

... Assume continuous thrust transfer to transfer orbit apogee using EP device, final orbit insertion using high thrust kick motor

... compare algorithm performance as Time interval ΔT becomes progressively larger

... Is there a point where algorithm blows up?

a.3) Continuous Small Thrust, Simulation to Hohmann Transfer Comparisons (*1 pt*)

... compare continuous thrust propellant mass calculations against Hohmann transfer calculations .. Assuming impulsively delivered Delta V for each burn

Burn 1: $I_{sp} = 2000 \text{ sec}$

Burn 2: $I_{sp} = 270 \text{ sec}$

... what can you conclude about the accuracy of the rocket equations and the impulsive Delta V assumption when applied to a long duration non-impulsive burn?

a.3) Impulsive Hohmann Transfer ...

Burn 2

Hohmann Transfer:

$$I_{sp} = 270 \text{ sec}$$

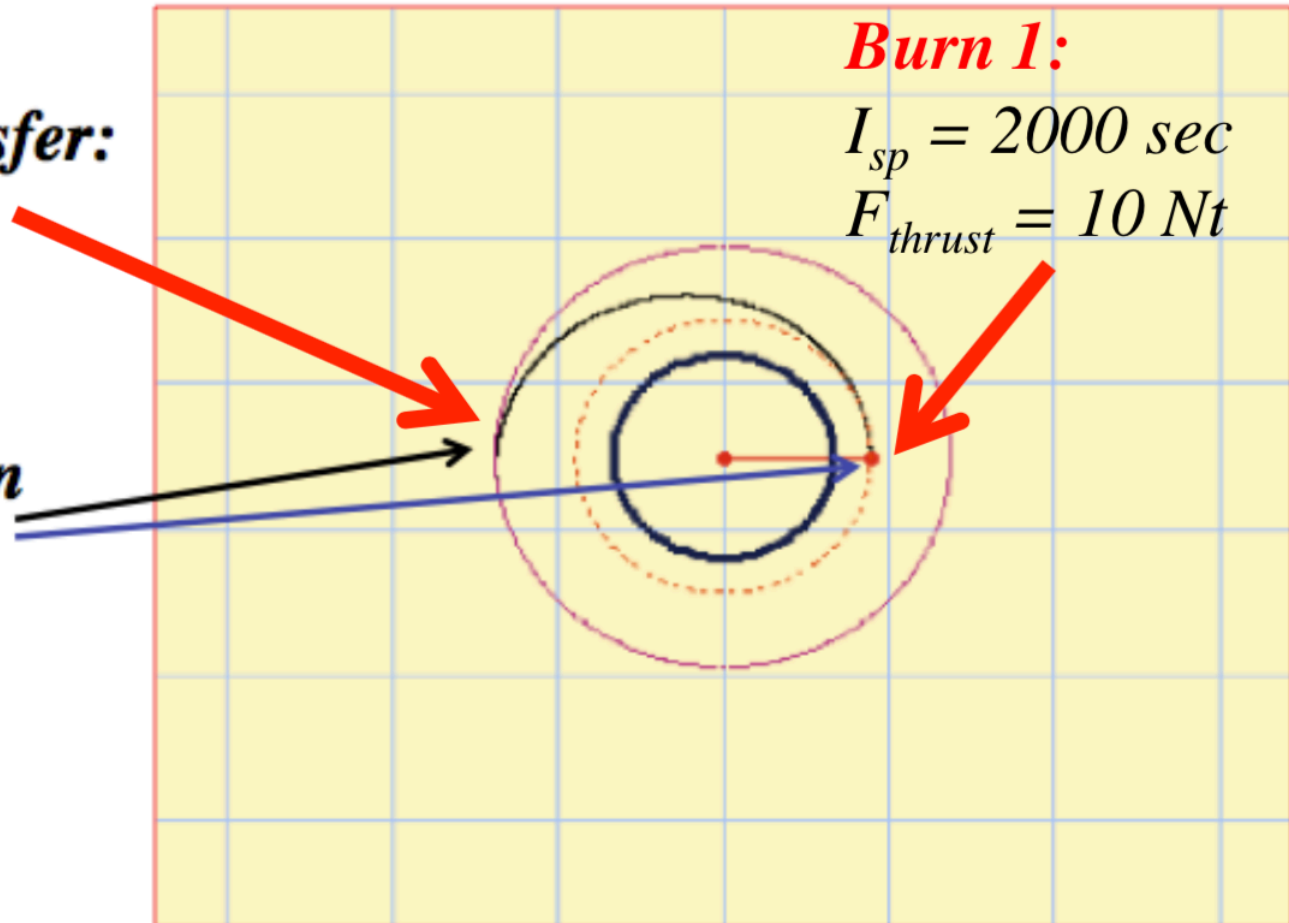
$$F_{thrust} = 2000 \text{ Nt}$$

• **Impulsive Burn Calculations**

Burn 1:

$$I_{sp} = 2000 \text{ sec}$$

$$F_{thrust} = 10 \text{ Nt}$$



- Calculate ΔV and Consumed Mass, Including Kick

Impulsive Hohmann Transfer (cont'd)

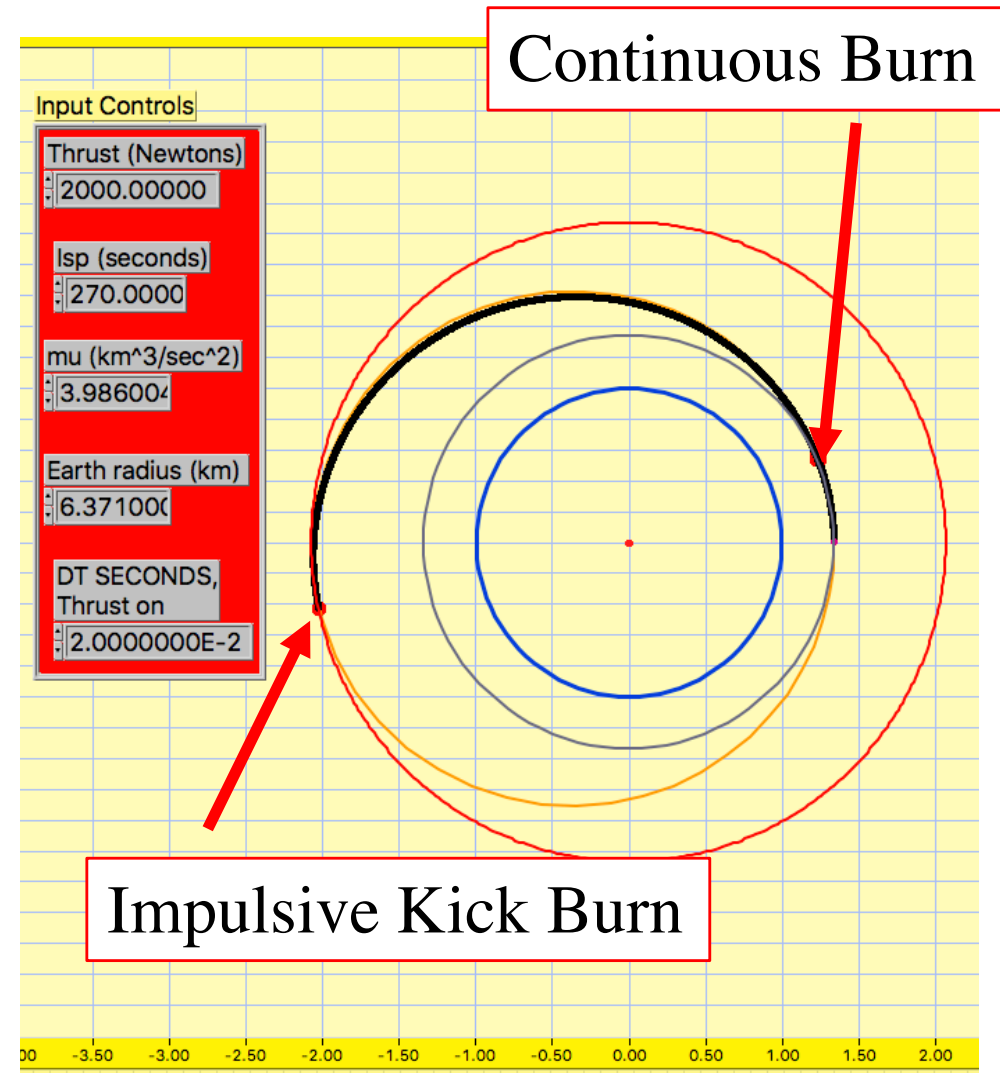
.... Small thrust transfer comparison

- Compare to continuous thrust transfer

	Propellant Mass kg	Propellant Mass kg
	Continuous Thrust Transfer	Impulsive Thrust Transfer
Burn 1 $I_{sp} = 2000 \text{ sec}$ $F = 10 \text{ N}$		
Burn 2 $I_{sp} = 270 \text{ sec}$ $F = 2000 \text{ N}$		
Total		

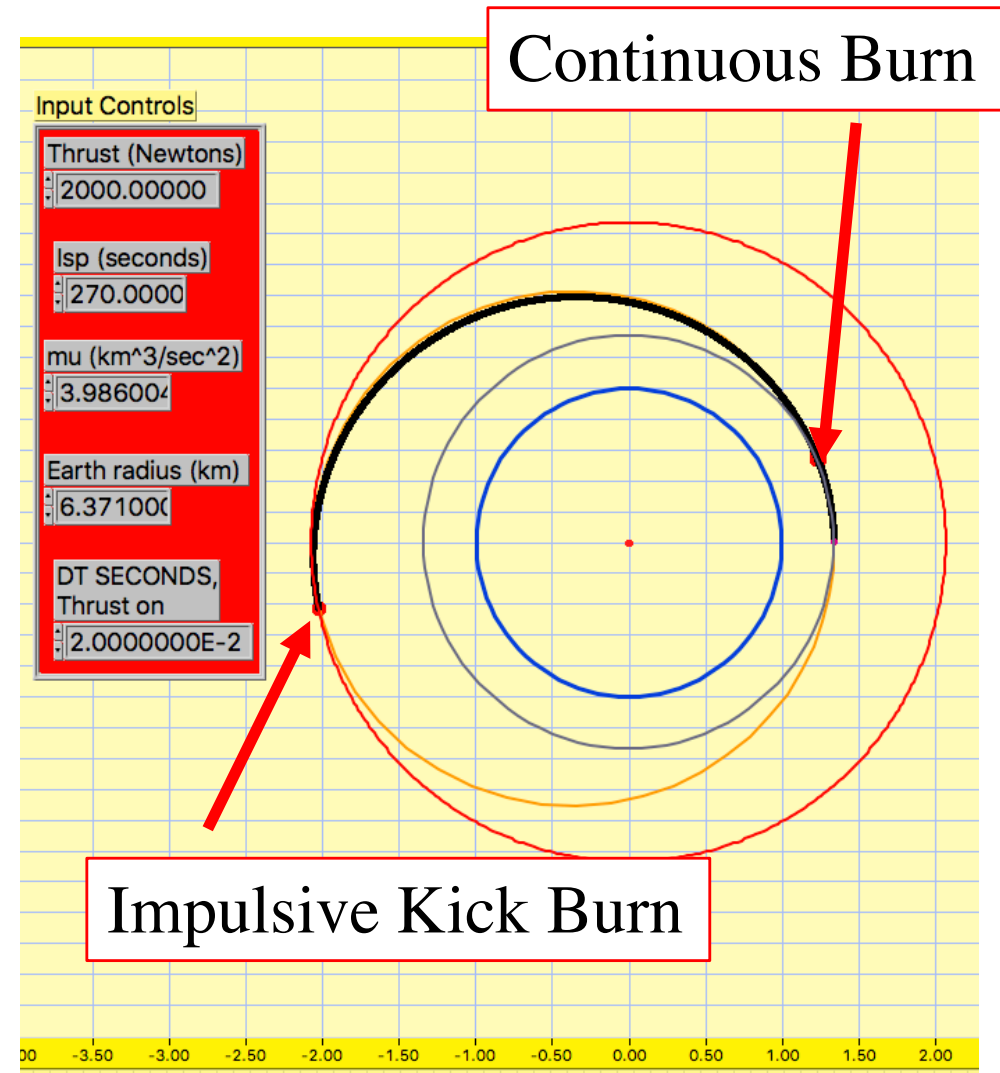
Part b.1) Continuous Large Thrust Analysis (3 pts)

- $F = 2000 \text{ N}$, $I_{sp} = 270 \text{ sec}$
- *Continuous First Burn*
- Terminate Thrust
When $a \cdot (1+e) \sim 13,200 \text{ km}$
- *Impulsive Second (Kick) Burn*
- Required $M_{final} = 1000 \text{ kg}$



Part b.1) Continuous Large Thrust Analysis

- → Calculate
- Propellant Mass Required for *Continuous* Transfer Burn
- ΔV , Propellant Mass Required for *Impulsive* Final Kick Burn
- $M_{final} = 1000 \text{ kg}$



Part b.2) Large Thrust Hohmann Transfer Analysis (*1 pt*)

... compare continuous thrust propellant mass and ΔV Calculations against Hohmann transfer calculations .. Assuming impulsively delivered Delta V for each burn

Burn 1: $I_{sp} = 270 \text{ sec}$

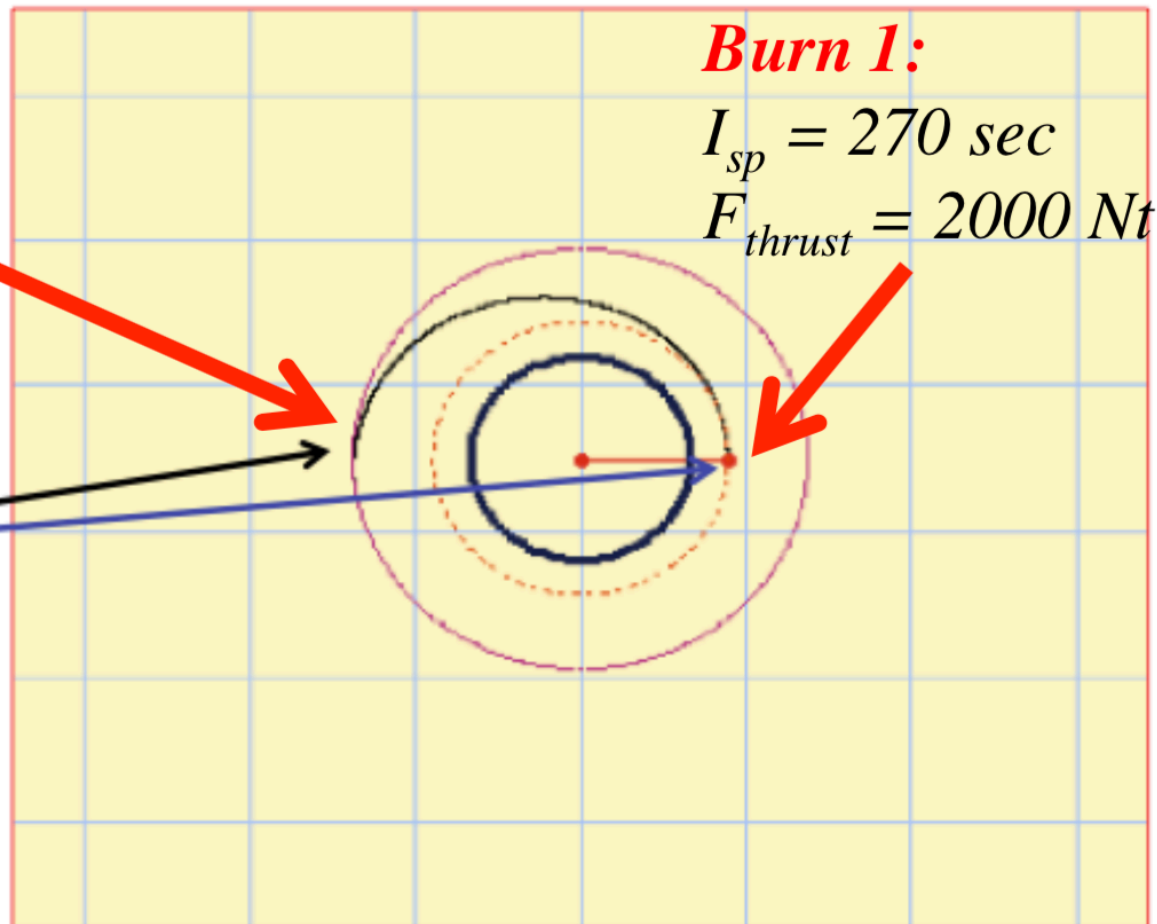
Burn 2: $I_{sp} = 270 \text{ sec}$

... what can you conclude about the accuracy of the rocket equations and the impulsive Delta V assumption when applied to a long Short-Duration (compared to orbit Period), Non-impulsive burn

Part b.2) Large Thrust Hohmann Transfer Analysis

Burn 2
Hohmann Transfer:
 $I_{sp} = 270 \text{ sec}$
 $F_{thrust} = 2000 \text{ Nt}$

• **Impulsive Burn
Calculations**



Part b) Large Thrust Hohmann Transfer Analysis

- Compare to one-burn continuous thrust transfer

	Propellant Mass kg	Propellant Mass kg
	Continuous Thrust Transfer	Impulsive Thrust Transfer
Burn 1 $I_{sp} = 270 \text{ sec}$ $F = 2000 \text{ N}$		
Burn 2 $I_{sp} = 270 \text{ sec}$ $F = 2000 \text{ N}$		266.80 kg
Total		

• **Part c.1) Two-Burn Grand Challenge (2 pts)**

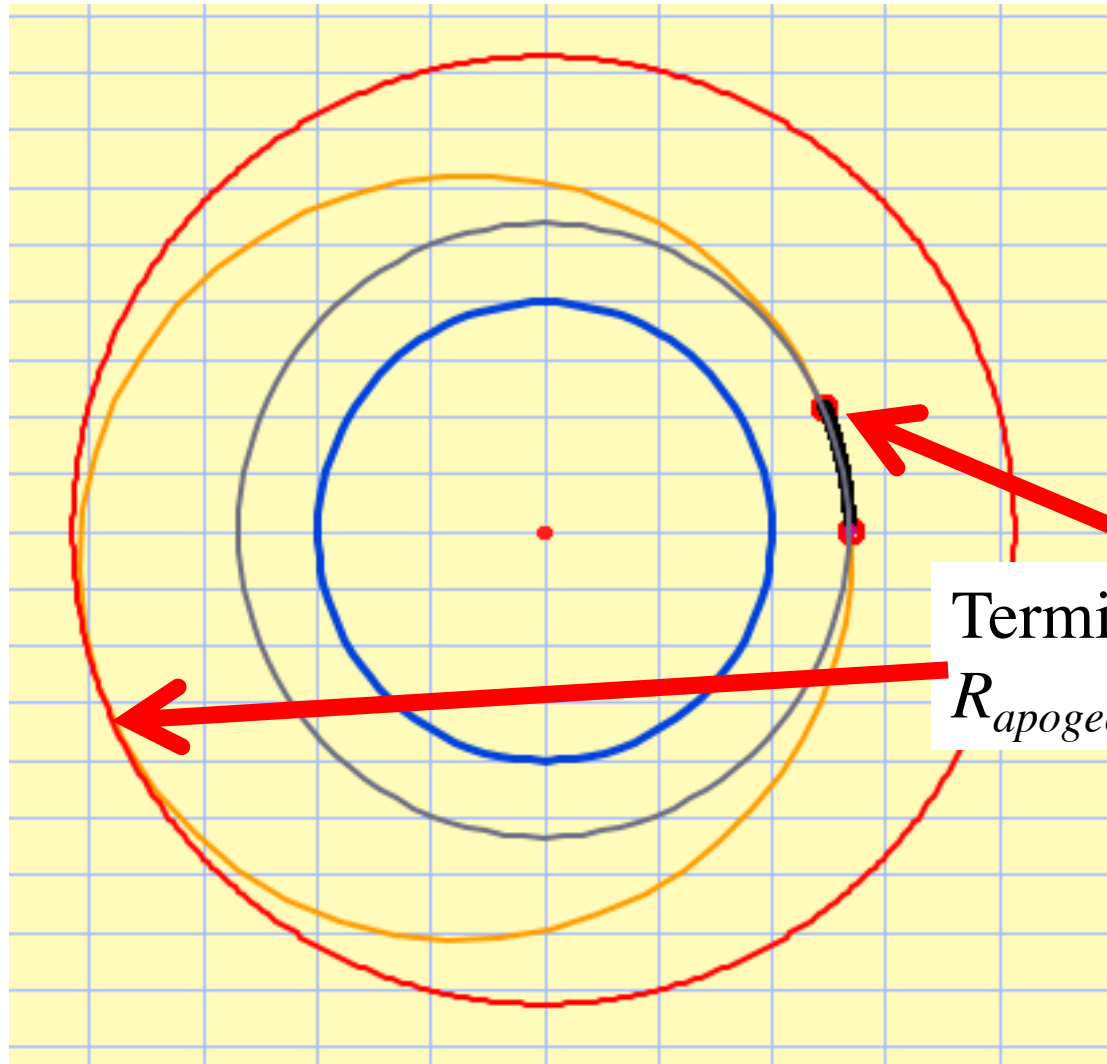
- **Assume BOTH burns are performed non-impulsively**
Terminate burn thrust when

Terminate Burn 1 Thrust When

$$R_{apogee} = a \cdot (1+e) \sim 13,200 \text{ km}$$

- **You decide** when and how long to initiate the second burn to circularize the orbit
- **Assume for large thrust 2000 Nt thrust (both burns) ... Isp = 270 sec**
- **Calculate required propellant mass for Burn1, Burn2 (and Total)**
- **Use integrator of your choice ... calculate actual delivered Delta V**
Based on consumed mass ... using rocket equation

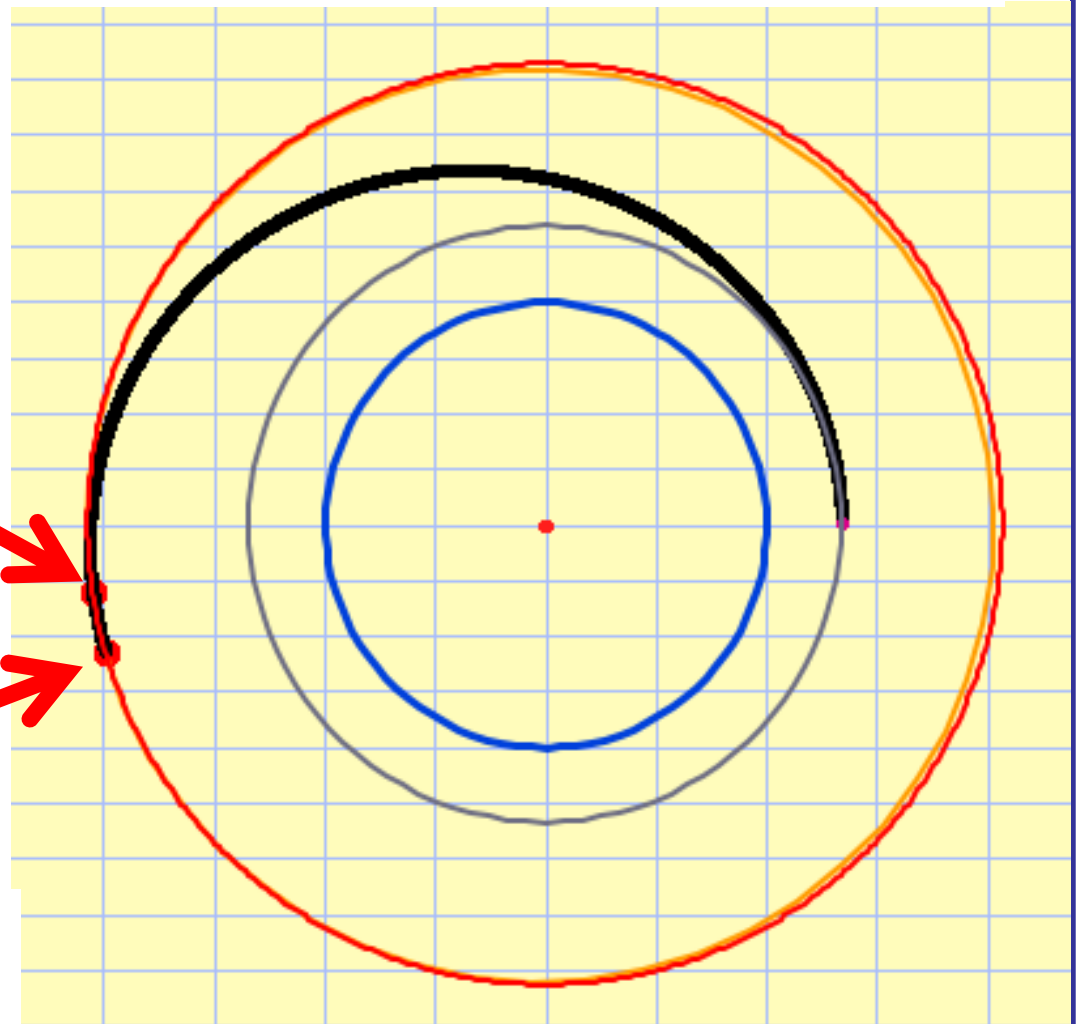
- Part c.1) Grand Challenge



Terminate Burn 1 Thrust When
 $R_{apogee} = a \cdot (1+e) \sim 13,200 \text{ km}$

• Part c.1) Two-Burn Grand Challenge

- You Decide When (or Where) to Initiate Second Burn



- Terminate Burn 2 Thrust Final Orbit $R_{apogee} \sim 13,200 \text{ km}$

- **Continuous Large Thrust Problem**

c.2) Final Summary (1 pt)

... compare Hohmann Transfer for 2000 Nt Rocket (assuming impulsive thrust) Versus 2000 Nt rocket with Non Impulsive Thrust Also compare consumed masses to High I_{sp} Continuous Thrust transfer

... what can you conclude about the accuracy of the rocket equation and the impulsive Delta V assumption when applied to a short duration non-impulsive burn?

... what can you conclude about the effect of I_{sp} on required propellant mass?

Impulsive Hohmann Transfer (cont'd)

....Large thrust transfer comparison

- Compare to two-burn continuous thrust transfer

	Propellant Mass kg		Propellant Mass kg	
	Continuous Thrust Transfer		Impulsive Thrust Transfer	
Burn 1 $I_{sp} = 270 \text{ sec}$ $F = 2000 \text{ N}$				
Burn 2 $I_{sp} = 270 \text{ sec}$ $F = 2000 \text{ N}$				
Total				

*+ 1 Point for neatness and completeness of
presentation/report*

Project hints

Collected Equations, Ballistic Trajectory

$$\begin{bmatrix} \dot{V}_r \\ \dot{V}_v \\ \dot{r} \\ \dot{v} \\ \dot{m} \end{bmatrix} = \begin{bmatrix} \frac{V_v^2}{r} - \frac{\mu}{r^2} + \left[\frac{F_{thrust}}{m} - \frac{\rho V_\infty^2}{2\beta} \right] \sin(\gamma) \\ -\frac{V_r V_v}{r} + \left[\frac{F_{thrust}}{m} - \frac{\rho V_\infty^2}{2\beta} \right] \cos(\gamma) \\ V_r \\ \frac{V_v}{r} \\ -\frac{F_{thrust}}{g_0 I_{sp}} \end{bmatrix} \alpha=0$$

$$\gamma = \tan^{-1} \left[\frac{V_r}{V_v} \right]$$

Ignore Drag

$$\beta = \sim \infty$$

$$\dot{X} = f[X, F_{thrust}]$$

Project Hints (1)

Position within initial orbit:

$$\begin{bmatrix} r \\ v \end{bmatrix}_0 = \begin{bmatrix} \frac{a_0(1 - e_0^2)}{1 + e_0 \cos(\nu_0)} \\ \nu_0 \end{bmatrix} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_0 = 0 \\ \text{can assume} \rightarrow \nu_0 = 0 \rightarrow a_0 = r_0 \end{bmatrix}$$

Angular velocity within initial orbit:

$$\omega_0 = \frac{\sqrt{\mu} [1 + e_0 \cos(\nu_0)]^2}{[a_0(1 - e_0^2)]^{3/2}} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_0 = 0 \\ \text{can assume} \rightarrow \nu_0 = 0, a_0 = r_0 \end{bmatrix}$$

$$\omega_0 = \frac{\sqrt{\mu} [1 + e_0 \cos(\nu_0)]^2}{[a_0(1 - e_0^2)]^{3/2}} = \frac{1}{r_0} \sqrt{\frac{\mu}{r_0}}$$

Project Hints (2)

Linear Velocity within initial orbit:

$$\begin{bmatrix} V_r \\ V_v \end{bmatrix}_0 = r_0 \omega_0 \begin{bmatrix} \frac{e_0 \sin[v_0]}{[1 + e_0 \cos(v_0)]} \\ 1 \end{bmatrix} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_0 = 0 \\ \text{can assume} \rightarrow v_0 = 0, a_0 = r_0 \end{bmatrix}$$

$$\begin{bmatrix} V_r \\ V_v \end{bmatrix}_0 = \begin{bmatrix} 0 \\ r_0 \omega_0 \end{bmatrix} = \begin{bmatrix} 0 \\ \sqrt{\frac{\mu}{r_0}} \end{bmatrix}$$

Project Hints (3)

Instantaneous (no-nonconservative forces acting) Keplerian orbit \rightarrow given: $\begin{bmatrix} V_r \\ V_v \end{bmatrix}, \begin{bmatrix} r \\ v \end{bmatrix}$

$$a = \frac{\mu}{\left[\frac{2\mu}{r} - [V_r^2 + V_v^2] \right]}$$

$$e = \frac{r}{\mu} \sqrt{\left(V_v^2 - \frac{\mu}{r} \right)^2 + (V_r V_v)^2}$$

$$r_{perigee} = a(1 - e)$$

$$r_{apogee} = a(1 + e)$$