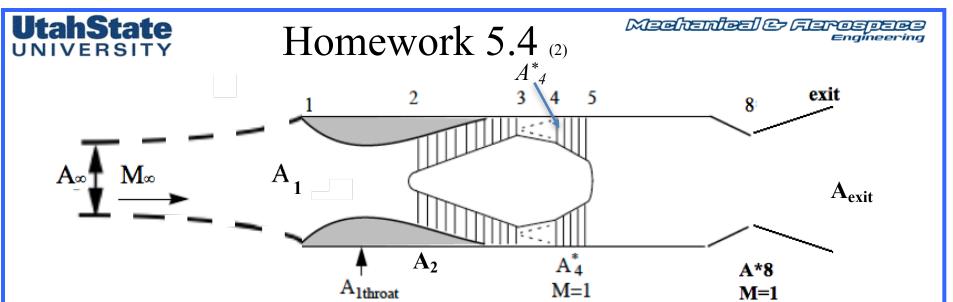


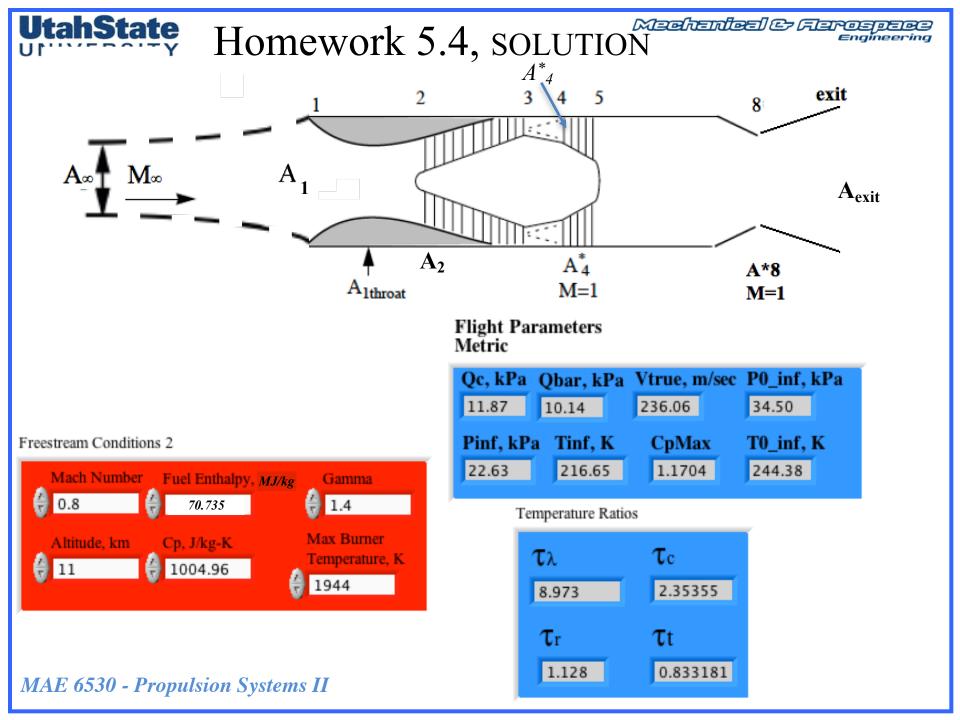
- Engine operates at a free stream Mach number, $M_{\infty} = 0.8$.
- Cruise Altitude is in the stratosphere, 11 km so $T_{\infty} = 216.65$ K.
- The design turbine inlet temperature, $T_{04} = 1944 K$
- The design compressor ratio, $\pi_c = 20$.
- Relevant area ratios are $A_2/A_4^* = 10$ and $A_2/A_{1throat} = 1.2$.
- Inlet throat area $A_{1Throat} = 20 \text{ cm}^2$
- Assume the compressor, burner and turbine all operate ideally.
- Nozzle is of a simple converging type with choked throat, $A^*_8 = A_{exit}$
- Stagnation pressure losses due to wall friction in the inlet and nozzle are negligible.
- → CALCULATE
- \rightarrow a) Correct Compressor Massflow and M_2 at compressor face
- \rightarrow b) Normalized exit pressure thrust, momentum thrust, and total thrust
- \rightarrow c) Velocity ratio across Engine V_{exit}/V_{∞}
- \rightarrow d) Mach number at diffuser throat, $M_{1throat}$
- → e) Inlet capture area
- → f) Total Thrust, Isp, TSFC

 $f \simeq 50$

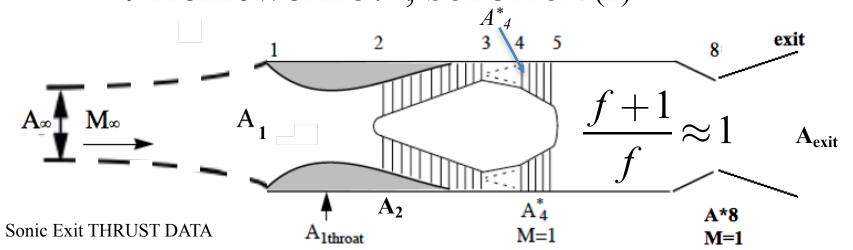
• Calculate Associated Fuel Enthalpy



- Now allow an expandable *Nozzle where*, $A_{exit} \ge A_{8}^{*}$
- \rightarrow CALCULATE
- \rightarrow a) Optimal expansion ratio for nozzle $A_{exit} \angle A_{8}^{*}$
- \rightarrow b) c) Velocity ratio across Engine $V_{\text{exit}}/V_{\infty}$
- \rightarrow c) thrust, Isp, TSFC of optimal nozzle,
- \rightarrow d) Assuming the same combustor temperature and inlet throat area as previous page
 - \rightarrow At what compressor demand π_c does the inlet throat choke (@ A1_{throat})
 - → Plot the Compressor operating line → π_c vs corrected massflow, $f(M_2)$ for $1 \le \pi_c < \pi_c$ @ choke
 - → Plot the capture area A_{∞} vs corrected massflow, $f(M_2)$ for $1 \leq \pi_c < \pi_c$ @ choke



UtahState Homework 5.4, SOLUTION (2)



- → CALCULATE
- \rightarrow a) Corrected Compressor massflow and M_2 at compressor face

mdot_COR g/SEC FM2 M2 402.505 0.695209 0.454202 *f* <u>∼</u> 50

→ b) Normalized exit pressure thrust, momentum thrust, and total thrust

	Norm Pressure Thrust	Normalized Momentum Thrust	Norm Total Thrust	Norm Isp	True Isp, sec	
	1.79721	1.95546	3.75267	167.53	5040.76	
\rightarrow	c) Velocity ratio across Engine $V_{ m exit}/V_{ m \infty}$		\rightarrow d) Mach number at diffuser throat, $M_{Ithroat}$			
	Ve/V∞		M1 t			
	3.12003		0.591318	A∞, cm^2	!	
			\rightarrow e) Inlet capture area	17.3229		

 $\frac{1}{f} = \frac{\tau_{\lambda} - \tau_{r} \cdot \tau_{c}}{\tau_{f} - \tau_{\lambda}}$ Calculate Fuel Enthalpy

Solve for
$$au_f$$

$$\rightarrow \frac{h_f}{c_p \cdot T_\infty} = \tau_f = \tau_\lambda + f \cdot \left(\tau_\lambda - \tau_r \cdot \tau_c\right)$$

Fuel-to-Airflow Matching

folve for
$$h$$
 .

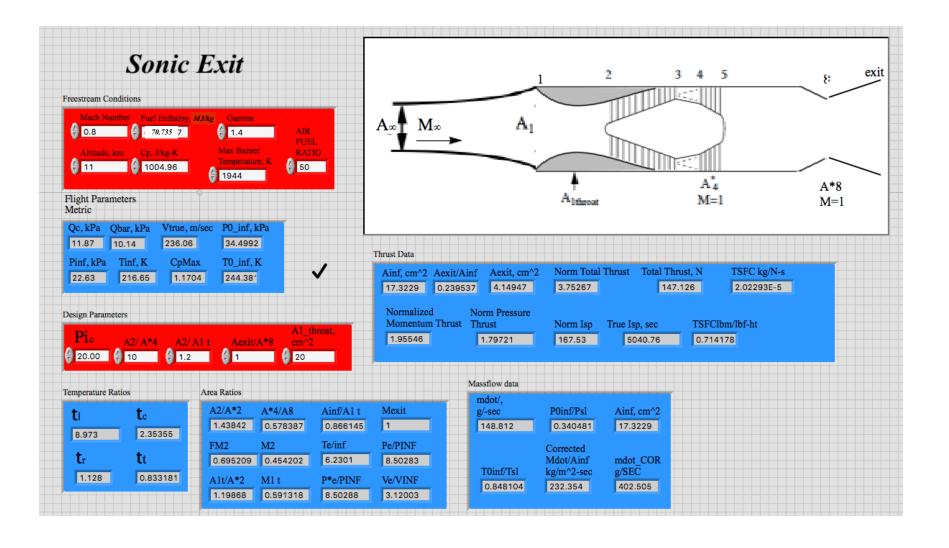
Solve for h_{f}

$$_{\sim}\cdot\left[\boldsymbol{\tau}_{\scriptscriptstyle{\lambda}}+\boldsymbol{f}\cdot\!\left(\boldsymbol{\tau}_{\scriptscriptstyle{\lambda}}-\boldsymbol{\tau}_{\scriptscriptstyle{r}}\cdot\boldsymbol{\tau}_{\scriptscriptstyle{c}}\right)\right]\!=\!$$

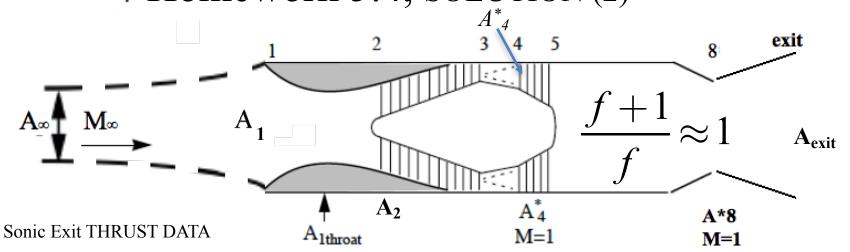
 $\rightarrow h_f = c_p \cdot T_\infty \cdot \left[\tau_\lambda + f \cdot \left(\tau_\lambda - \tau_r \cdot \tau_c \right) \right] = 0$

 $1004.96_{J/kg-K} \cdot 216.65_{K} \cdot [8.973 + 50 \cdot (9.973 - 1.128 \cdot 2.25355)] =$

 $70.735_{MJ/kg}$ Wow! hot stuff!

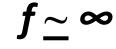


UtahState Homework 5.4, SOLUTION (2)



- \rightarrow CALCULATE
- \rightarrow a) Corrected Compressor massflow and M_2 at compressor face

mdot_COR g/SEC FM2 M2 410.547 0.709099 0.466242



→ b) Normalized exit pressure thrust, momentum thrust, and total thrust

Norm Pressure Thrust		Normalized Momentum Thrust		Norm Total Thrust	
	1.75516	1.89401		3.64917	

⇒ c) Velocity ratio across Engine V_{exit}/V_{∞} Ve/V ∞ 3.11379

→ d) Mach number at diffuser throat, $M_{1throat}$ M1 t

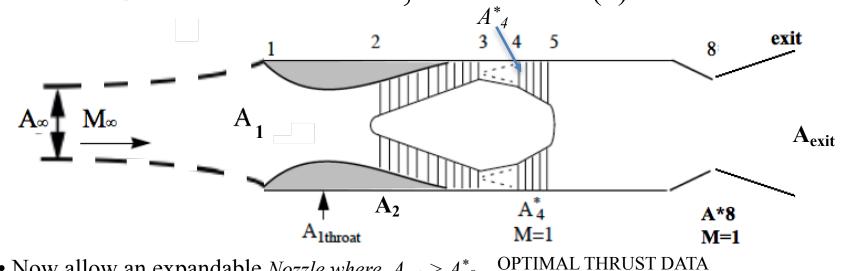
O.611294

A∞, cm^2

 \rightarrow e) Inlet capture area

17.669

UtahState Homework 5.4, SOLUTION (3)



- Now allow an expandable *Nozzle where*, $A_{exit} \ge A_{8}^{*}$
- \rightarrow CALCULATE
- \rightarrow a) Optimal expansion ratio for nozzle $A_{\text{exit}} / A_{8}^{*}$

Pe/P∞ Aexit/A*8

1 → Aexit/A*8

2.54417

 \rightarrow b) c) Velocity ratio across Engine $V_{\text{exit}}/V_{\infty}$

Ve/V∞ 5.657

 \rightarrow c) thrust of optimal nozzle

 $f \sim 50$ Total Thrust, N

Norm Isp True Isp, sec 190.806 5741.11

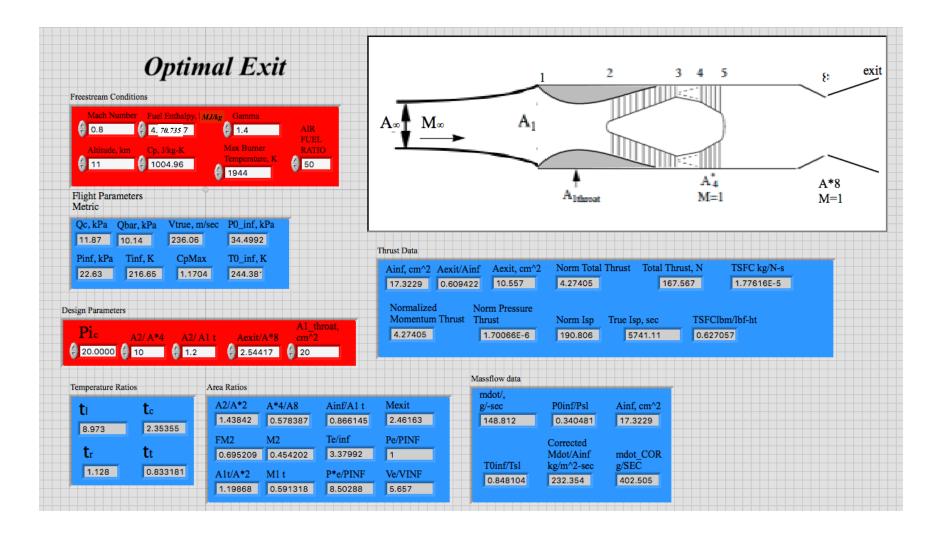
Aexit/A∞
0.609422

Norm Pressure
Thrust
1.70066E-6

Normalized Momentum Thrust Norm Total Thrust

4.27405

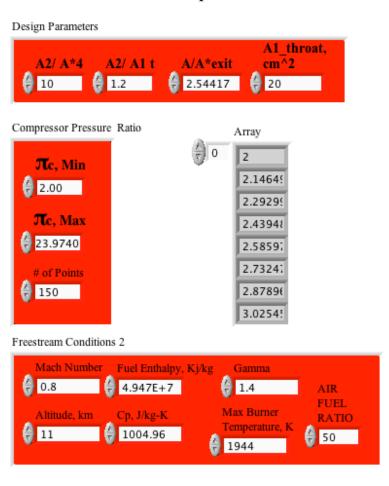
4.27405

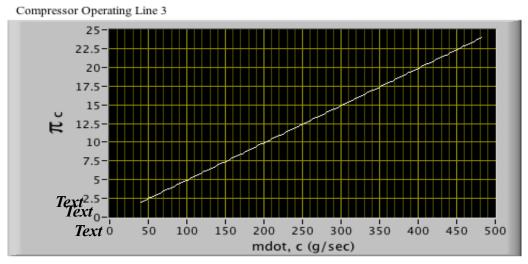


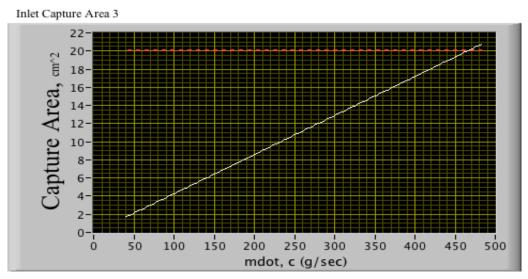


Homework 5.4, SOLUTION (4)

- → d) Assuming the same combustor temperature and inlet throat area
 - \rightarrow Plot the Compressor operating line $\rightarrow \pi_c$ vs corrected massflow for $1 \le \pi c < Choke$
 - \rightarrow Plot the capture area A_{∞} vs corrected massflow for $1 \leq \pi c < Choke$



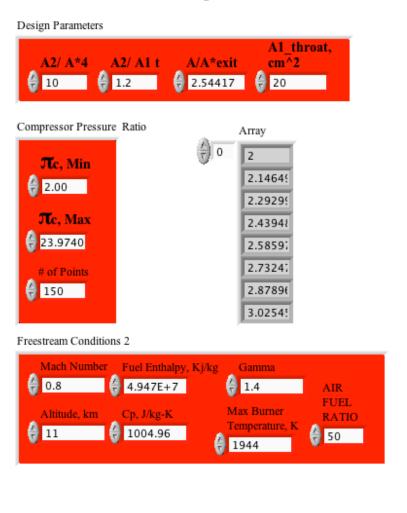


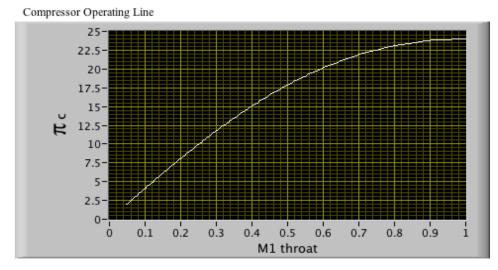


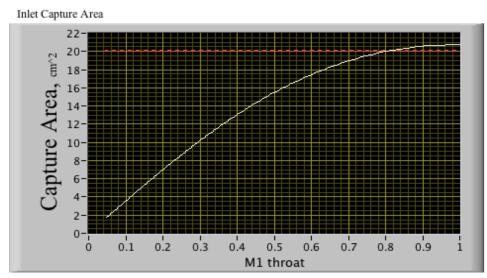


Homework 5.4, SOLUTION (4)

- \rightarrow d) Assuming the same combustor temperature and inlet throat area
 - \rightarrow Plot the Compressor operating line $\rightarrow \pi_c$ vs corrected massflow for $1 \le \pi c < Choke$
 - → Plot the capture area A_{∞} vs corrected massflow for $1 \leq \pi c < Choke$









Homework 5.4, SOLUTION (4)

- \rightarrow d) Assuming the same combustor temperature and inlet throat area
 - → Plot the Compressor operating line → π_c vs corrected massflow for $1 \le \pi c < Choke$
 - → Plot the capture area A_{∞} vs corrected massflow for $1 \leq \pi c < Choke$

